Introduction to continuum mechanics-II

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Continuum kinematics

- *B*₀ undeformed/reference configuration, *B*_t deformed/actual configuration
- Motion: $\boldsymbol{x}(t, \boldsymbol{X}) = \boldsymbol{X} + \boldsymbol{u}(t, \boldsymbol{X})$ with $\boldsymbol{x}(t, \boldsymbol{\mathcal{B}}_0) = \boldsymbol{\mathcal{B}}_t$.
- Material/Lagrangian coordinates: $m{X} = (X_1, X_2, X_3) \in m{\mathcal{B}}_0$
- Spatial/Eulerian coordinates: $\boldsymbol{x} = (x_1, x_2, x_3) \in \boldsymbol{\mathcal{B}}_t$
- u(t, X) = x(t, X) X the displacement field



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Velocity-acceleration

- velocity (in Lagrange variables) $\boldsymbol{v}(t, \boldsymbol{X}) = \frac{\partial \boldsymbol{x}}{\partial t}(t, \boldsymbol{X})$
- Suppose $X \to x(t, X)$ one to one function, then $\exists x \to X(t, x)$
- velocity (in Euler variables) $\boldsymbol{v}(t, \boldsymbol{x}) = \boldsymbol{v}(t, \boldsymbol{X}(t, \boldsymbol{x})).$
- acceleration (in Lagrange variables) $\boldsymbol{a}(t, \boldsymbol{X}) = \frac{\partial^2 \boldsymbol{x}}{\partial^2 t}(t, \boldsymbol{X})$
- acceleration (in Euler variables) $\boldsymbol{a}(t, \boldsymbol{x}) = \boldsymbol{a}(t, \boldsymbol{X}(t, \boldsymbol{x})).$

Example. Dilatation:

- $x_1 = X_1 + \alpha_1 t X_1, \quad x_1 = X_2 + \alpha_2 t X_2, \quad x_3 = X_3 + \alpha_3 t X_3$
 - velocity (in Lagrange variables) $\boldsymbol{v}(t, \boldsymbol{X}) = (\alpha_1 X_1, \alpha_2 X_2, \alpha_3 X_3)$
 - velocity (in Euler variables) $\boldsymbol{v}(t, \boldsymbol{x}) = \left(\frac{\alpha_1}{1+\alpha_1 t} x_1, \frac{\alpha_2}{1+\alpha_2 t} x_2, \frac{\alpha_3}{1+\alpha_3 t} x_3\right).$

Particular (material, total) derivative

Particular (total) derivative of field K (the particle is followed in its movement) : $K(t, \mathbf{X})$ in Lagrange description, $K(t, \mathbf{x}) = K(t, \mathbf{X}(t, \mathbf{x}))$ in Eulerian description

• if K is in Lagrange variables
$$\frac{dK}{dt}(t, \mathbf{X}) = \frac{\partial K}{\partial t}(t, \mathbf{X})$$

• if K is in Euler variables $\frac{dK}{dt}(t, \mathbf{x}) = \frac{\partial K}{\partial t}(t, \mathbf{x}) + \mathbf{v}(t, \mathbf{x}) \cdot \nabla_{\mathbf{x}} K(t, \mathbf{x})$
Examples

•
$$K = \mathbf{x}$$
: $\frac{d\mathbf{x}}{dt}(t, \mathbf{x}) = \mathbf{v}(t, \mathbf{x})$
• $K = \mathbf{v}(t, \mathbf{x})$: $\frac{d\mathbf{v}}{dt}(t, \mathbf{x}) = \mathbf{a}(t, \mathbf{x}) = \frac{\partial \mathbf{v}}{\partial t}(t, \mathbf{x}) + \mathbf{v}(t, \mathbf{x}) \cdot \nabla_{\mathbf{x}} \mathbf{v}(t, \mathbf{x})$

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Reynolds's transport theorem

Particular (material, total) derivative of a volume integral Let $\omega_0 \subset \mathcal{B}_0$ and $\omega_t = \mathbf{x}(t, \omega_0) \subset \mathcal{B}_t$ (the subset $\omega_0 \subset \mathcal{B}_0$ is followed in its movement) and $K(t, \mathbf{x})$ a field in Eulerian description

$$\frac{d}{dt} \int_{\omega_t} K(t, \mathbf{x}) \, d\mathbf{x} = \int_{\omega_t} \left(\frac{\partial K}{\partial t}(t, \mathbf{x}) + \operatorname{div}_{\mathbf{x}}(K(t, \mathbf{x})\mathbf{v}(t, \mathbf{x})) \right) \, d\mathbf{x}$$
$$= \int_{\omega_t} \frac{dK}{dt}(t, \mathbf{x}) + K(t, \mathbf{x}) \operatorname{div}_{\mathbf{x}} \mathbf{v}(t, \mathbf{x}) \, d\mathbf{x} = \int_{\omega_t} \frac{\partial K}{\partial t}(t, \mathbf{x}) + \int_{\partial \omega_t} K(t, \mathbf{x}) \mathbf{v}(t, \mathbf{x}) \cdot \mathbf{n} \, d\mathbf{x}$$

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Examples

•
$$K \equiv 1$$
: $\frac{d}{dt} Vol(\omega_t) = \int_{\omega_t} div_{\mathbf{x}} \mathbf{v}(t, \mathbf{x}) d\mathbf{x} = \int_{\partial \omega_t} \mathbf{v}(t, \mathbf{x}) \cdot \mathbf{n} dS$

• if $div_{\mathbf{x}}\mathbf{v}(t,\mathbf{x}) = 0$ then the volume is incompressible

Kinematics Deformation

Deformation of a continuous body



- infinitesimal element of a continuous body $d\mathbf{X} = (dX_1, dX_2, dX_3)$
- It is possible to show that (using Taylor expansion around a point of deformation)

$$d\mathbf{x} = \mathbf{F}(t, \mathbf{X}) d\mathbf{X} = (\mathbf{I} + \nabla \mathbf{u}(t, \mathbf{x})) d\mathbf{X}$$

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$$dx_i = F_{ik} dX_k = (\delta_{ik} + \frac{\partial u_i}{\partial X_k}) dX_k$$

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Volume change

- Consider a differential material volume dV at some material point that goes to dv after deformation
- How to measure the volume change ?
- Reference volume: $dV_0 = d\mathbf{Z} \cdot (d\mathbf{X} \times d\mathbf{Y})$
- Deformed volume: $dv = d\mathbf{W} \cdot (d\mathbf{R} \times d\mathbf{V})$
- $J(t, \mathbf{X}) = det(\mathbf{F}(t, \mathbf{X}))$ Jacobien of the trasformation
- It is easy to show that the volume change: dv = JdV



Polar decomposition theorem

- A rotation matrix: **R** such that $\mathbf{R}\mathbf{R}^{T} = \mathbf{R}^{T}\mathbf{R} = \mathbf{I}$ (det $\mathbf{R} = I$).
- Polar decomposition theorem: For any matrix F with detF > 0, there exists an unique rotation R and an unique positive-definite symmetric matrix U such that

$$F = RU$$

• how to calculate it ? Calculate the Cauhy-Green strain tensor $C = F^T F$ and then $U = \sqrt{C}$, i.e. Find the eigenvalues $\{\gamma_1, \gamma_2, \gamma_3\}$ and eigenvectors $\{u_1, u_2, u_3\}$ of C calculate $\mu_i = \sqrt{\gamma_i}$ and then Uis the matrix with eigenvalues $\{\mu_1, \mu_2, \mu_3\}$ and the corresponding eigenvectors such that

$$\boldsymbol{U} = \mu_1 \boldsymbol{u}_1 \otimes \boldsymbol{u}_1 + \mu_2 \boldsymbol{u}_2 \otimes \boldsymbol{u}_2 + \mu_3 \boldsymbol{u}_3 \otimes \boldsymbol{u}_3$$

$$\mathbf{R} = \mathbf{F} \mathbf{U}^{-1}$$

Geometric modeling: an Eulerian approach Conservation laws

Kinematics Deformation

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Polar decomposition theorem



Velocity gradient

Velocity gradient tensor $\boldsymbol{L} = \boldsymbol{L}(t, \boldsymbol{x}) = \nabla_{\boldsymbol{x}} \boldsymbol{v}(t, \boldsymbol{x}), \quad L_{ij} = \frac{\partial v_i}{\partial x_i}$

$$\boldsymbol{L} = \dot{\boldsymbol{F}}\boldsymbol{F}^{-1} = (\frac{d}{dt}\boldsymbol{F})\boldsymbol{F}^{-1}$$
$$\boldsymbol{L} = \dot{\boldsymbol{R}}\boldsymbol{R}^{T} + \boldsymbol{R}\dot{\boldsymbol{I}}\boldsymbol{I}\boldsymbol{I}^{-1}\boldsymbol{R}^{T}$$

Strain rate (stretching, rate of deformation) tensor D = D(v)

$$\boldsymbol{D} = \boldsymbol{D}(t, \boldsymbol{x}) = \frac{1}{2} (\nabla_{\boldsymbol{x}} \boldsymbol{v}(t, \boldsymbol{x}) + \nabla_{\boldsymbol{x}}^{T} \boldsymbol{v}(t, \boldsymbol{x})), \quad D_{ij} = \frac{1}{2} (\frac{\partial v_{i}}{\partial x_{j}} + \frac{\partial v_{j}}{\partial x_{i}})$$

Spin tensor W = W(v)

$$W = W(t, \mathbf{x}) = \frac{1}{2} (\nabla_{\mathbf{x}} \mathbf{v}(t, \mathbf{x}) - \nabla_{\mathbf{x}}^{T} \mathbf{v}(t, \mathbf{x})), \quad W_{ij} = \frac{1}{2} (\frac{\partial v_{i}}{\partial x_{j}} - \frac{\partial v_{j}}{\partial x_{i}})$$
$$L = D + W, \quad D^{T} = D, \quad W^{T} = -W$$
$$\omega(t, \mathbf{x}) = curl_{\mathbf{x}} \mathbf{v}(t, \mathbf{x}), \quad W \mathbf{c} = \frac{1}{2} \omega \times \mathbf{c}, \quad \forall \mathbf{c}$$

Rate of Change of Length and Orientation.

$$d\mathbf{x} = \mathbf{F} d\mathbf{X}, \mathbf{L} = \dot{\mathbf{F}} \mathbf{F}^{-1} \Longrightarrow \frac{d}{dt} (d\mathbf{x}) = \mathbf{L} d\mathbf{x}$$

Orientation and length of the infinitesimal vectors

$$d\mathbf{x} = \mathbf{n} ds, d\mathbf{x}^1 = \mathbf{n}^1 ds^1, d\mathbf{x}^2 = \mathbf{n}^2 ds^2$$

Rate of change of orientation $\frac{d}{dt}(\mathbf{n}) = \mathbf{L}\mathbf{n} - (\mathbf{D}\mathbf{n} \cdot \mathbf{n})\mathbf{n}$

$$\frac{d}{dt}(d\boldsymbol{x}^1\cdot d\boldsymbol{x}^2) = 2\boldsymbol{D}\boldsymbol{x}^1\cdot d\boldsymbol{x}^2$$

Rate of change of length

$$d\mathbf{x}^1 = d\mathbf{x}^2 = \mathbf{n} ds \Longrightarrow \frac{d}{dt}(\ln ds) = \frac{1}{ds}\frac{d}{dt}(ds) = \mathbf{D}\mathbf{n} \cdot \mathbf{n}$$

Rate of change of angles

$$\frac{d}{dt}(\boldsymbol{n}^1 \cdot \boldsymbol{n}^2) = 2\boldsymbol{D}\boldsymbol{n}^1 \cdot \boldsymbol{n}^2 - (\boldsymbol{D}\boldsymbol{n}^1 \cdot \boldsymbol{n}^1 + \boldsymbol{D}\boldsymbol{n}^2 \cdot \boldsymbol{n}^2) \boldsymbol{n}^1 \cdot \boldsymbol{n}^2$$

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Mass conservation law

Let $\rho_0: \mathcal{B}_0 o \mathbb{R}_+, \text{and } \rho(t, \cdot): \mathcal{B}_t o \mathbb{R}_+$ be the mass density such that

$$\mathit{mass}(\omega_0) = \int_{\omega_0}
ho_0({m{X}}) \; d{m{X}}, \quad \mathit{mass}(\omega_t) = \int_{\omega_t}
ho(t, {m{x}}) \; d{m{x}}$$

for all $\omega_0 \subset \mathcal{B}_0$ and $\omega_t = \mathbf{x}(t, \omega_0) \subset \mathcal{B}_t$.

- Mass conservation law: $mass(\omega_0) = mass(\omega_t)$ for all $\omega_0 \subset \mathcal{B}_0$.
- Lagrangian description $ho(t, {m x}) J(t, {m X}) =
 ho_0({m X})$ for all ${m X} \in {m {\cal B}}_0$
- Eulerian description $\frac{d}{dt}
 ho(t, \mathbf{x}) +
 ho(t, \mathbf{x}) div_{\mathbf{x}} \mathbf{v}(t, \mathbf{x}) = 0$ for all $\mathbf{x} \in \mathcal{B}_t$
- Eulerian description $\frac{\partial}{\partial t}\rho(t, \mathbf{x}) + div_{\mathbf{x}}(\rho(t, \mathbf{x})\mathbf{v}(t, \mathbf{x})) = 0$

Consequence:
$$\frac{d}{dt} \int_{\omega_t} \rho(t, \mathbf{x}) K(t, \mathbf{x}) d\mathbf{x} = \int_{\omega_t} \rho(t, \mathbf{x}) \frac{d}{dt} K(t, \mathbf{x}) d\mathbf{x}$$

Geometric modeling: an Eulerian approach Conservation laws Mass conservation law Cauchy assumption and stress vectors Momentum balance law

Forces acting on the body



Assumptions

- Body forces $\rho \boldsymbol{b} d\boldsymbol{x}$: $\boldsymbol{b} = \boldsymbol{b}(t, \boldsymbol{x})$
- Surface forces tdS acting on ∂D_t: the action of B_t \ D_t on D_t can be replaced by the distribution of the Cauchy stress vector t
- Cauchy's hypothesis: t = t(t, x, n)

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The Balance of Momentum Principles

Balance principle for linear momentum (Newton's law):

$$\frac{d}{dt}\int_{\omega_t}\rho(t,\boldsymbol{x})\boldsymbol{v}(t,\boldsymbol{x}) d\boldsymbol{x} = \int_{\omega_t}\rho(t,\boldsymbol{x})\boldsymbol{b}(t,\boldsymbol{x}) d\boldsymbol{x} + \int_{\partial\omega_t}\boldsymbol{t}(t,\boldsymbol{x},\boldsymbol{n}) dS$$

Balance principle for angular momentum (Newton's law):

$$\frac{d}{dt}\int_{\omega_t}\rho(t,\mathbf{x})\mathbf{x}\wedge\mathbf{v}(t,\mathbf{x})\ d\mathbf{x} = \int_{\omega_t}\rho(t,\mathbf{x})\mathbf{x}\wedge\mathbf{b}(t,\mathbf{x})\ d\mathbf{x} + \int_{\partial\omega_t}\mathbf{x}\wedge\mathbf{t}(t,\mathbf{x},\mathbf{n})\ dS$$

for all $\omega_t \subset \mathcal{B}_t$.

Consequences of balance principles and stress tensor

Consequences of linear momentum balance principle + Cauchy's hypothesis

• $n \rightarrow t(t, x, n)$ is linear and there exists $\sigma(t, x)$ Cauchy stress tensor such that

$$t(t, x, n) = \sigma(t, x)n$$

Equation of motion

$$\rho(t, \mathbf{x}) \frac{d}{dt} \mathbf{v}(t, \mathbf{x}) = div_{\mathbf{x}} \sigma(t, \mathbf{x}) + \rho(t, \mathbf{x}) \mathbf{b}(t, \mathbf{x})$$

Consequence of angular momentum balance principle

• Cauchy stress tensor is symetric

$$\boldsymbol{\sigma}^{\mathsf{T}}(t,\boldsymbol{x}) = \boldsymbol{\sigma}(t,\boldsymbol{x})$$

Mass conservation law Cauchy assumption and stress vectors Momentum balance law

Equation of motion in Lagrange formulation

First Piola-Kirchhoff stress tensor (non-symmetric !)

$$\mathbf{\Pi}(t, \mathbf{X}) = J(t, \mathbf{X}) \boldsymbol{\sigma}(t, \mathbf{x}(t, \mathbf{X})) \boldsymbol{F}^{-T}(t, \mathbf{X})$$



Nanson's formula $\boldsymbol{n} dS = J \boldsymbol{F}^{-T} \boldsymbol{n}_0 dS_0 \Longrightarrow \boldsymbol{\sigma}(t, \boldsymbol{x}) \boldsymbol{n} dS = \boldsymbol{\Pi}(t, \boldsymbol{X}) \boldsymbol{n}_0 dS_0$

$$\rho_0(\boldsymbol{X}) \frac{d}{dt} \boldsymbol{v}(t, \boldsymbol{X}) = di v_{\boldsymbol{X}} \boldsymbol{\Pi}(t, \boldsymbol{X}) + \rho_0(\boldsymbol{X}) \boldsymbol{b}(t, \boldsymbol{X})$$

Equilibrium equation $div_{\mathbf{X}} \mathbf{\Pi}(t, \mathbf{X}) + \rho_0(\mathbf{X}) \mathbf{b}(t, \mathbf{X}) = 0$ Second Piola-Kirchhoff tensor (symmetric !) $\mathbf{S} = \mathbf{F}^{-1} \mathbf{\Pi}$

Mass conservation law Cauchy assumption and stress vectors Momentum balance law

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Examples of stress tensors